

**ECE452/552**

**HW #5**

**SOLUTION**

Question (4) is from Ogata, “Discrete-Time Control Systems” 2<sup>nd</sup> ed., page 292.

- 1) Obtain the discrete-time equivalent of the following continuous-time filter by the use of
  - (1) the backward difference method, and,
  - (2) the impulse-invariance method:

$$G(s) = \frac{2}{(s+1)(s+2)}$$

Assume that the sampling period is 0.1 sec, or  $T = 0.1$ .

- 2) Question 2 from the Midterm 2 practice exam:

Use the matched pole-zero mapping method to determine the equivalent discrete-time filter for the following:

$$G(s) = \frac{s+a}{s(s+b)}$$

- 3) For the above questions (1) and (2) use Matlab (using the ‘*bode*’ command) to compare the Bode plots of the continuous-time and discrete-time systems. For Question 2 use  $a = 1$ ,  $b = 10$  and sampling period,  $T = 0.2$ . So, for each of the three continuous-time and discrete-time frequency response pairs be sure to plot each pair on the same graph.
- 4) B-4-16 (from Ogata page 292)

.....

## SOLUTIONS:

### Question 1:

$$G(s) = \frac{2}{(s+1)(s+2)}$$

1. Backward difference method: To obtain  $G_D(z)$  we substitute

$$s = \frac{1 - z^{-1}}{T} = 10(1 - z^{-1})$$

into  $G(s)$ .

$$\begin{aligned} G_D(z) &= \frac{2}{(10 - 10z^{-1} + 1)(10 - 10z^{-1} + 2)} \\ &= \frac{0.01515}{1 - 1.7424z^{-1} + 0.7576z^{-2}} \end{aligned}$$

2. Impulse invariance method:

$$\begin{aligned} G_D(z) &= TG(z) = (0.1) \mathcal{Z} \left[ \frac{2}{(s+1)(s+2)} \right] \\ &= \frac{0.01722z^{-1}}{1 - 1.7235z^{-1} + 0.7408z^{-2}} \end{aligned}$$

### Question 2:

$$G(s) = \frac{s+a}{s(s+b)}$$

By use of the matched pole-zero mapping method, the equivalent discrete-time filter or digital filter can be obtained in the following form:

$$G_D(z) = K \frac{(z+1)(z - e^{-aT})}{(z-1)(z - e^{-bT})} = K \frac{(1+z^{-1})(1 - e^{-aT}z^{-1})}{(1 - z^{-1})(1 - e^{-bT}z^{-1})}$$

Since both  $G_D(1)$  and  $G(0)$  approach infinity, constant  $K$  cannot be determined by equating  $G_D(1)$  to  $G(0)$ . Therefore, we shall use the velocity error constant for determining constant  $K$ . For the analog filter

$$K_V = \lim_{s \rightarrow 0} sG(s) = \lim_{s \rightarrow 0} \frac{s+a}{s+b} = \frac{a}{b}$$

For the equivalent digital filter

$$\begin{aligned} K_V &= \lim_{z \rightarrow 1} \frac{1 - z^{-1}}{T} G_D(z) \\ &= \lim_{z \rightarrow 1} \frac{1 - z^{-1}}{T} K \frac{(1 + z^{-1})(1 - e^{-aT}z^{-1})}{(1 - z^{-1})(1 - e^{-bT}z^{-1})} = \frac{K}{T} \frac{2(1 - e^{-aT})}{1 - e^{-bT}} \end{aligned}$$

Equating the  $K_v$  values obtained above, we get

$$K = \frac{aT}{2b} \frac{1 - e^{-bT}}{1 - e^{-aT}}$$

Hence, the equivalent digital filter  $G_D(z)$  becomes as follows:

$$G_D(z) = \frac{aT}{2b} \frac{(1 - e^{-bT})}{(1 - e^{-aT})} \frac{(1 + z^{-1})(1 - e^{-aT}z^{-1})}{(1 - z^{-1})(1 - e^{-bT}z^{-1})}$$

Note that for sufficiently small values of  $T$  such that  $e^{-aT}$  and  $e^{-bT}$  can be approximated by

$$e^{-aT} \doteq 1 - aT \quad \text{and} \quad e^{-bT} \doteq 1 - bT$$

we have

$$K = \frac{aT}{2b} \frac{1 - e^{-bT}}{1 - e^{-aT}} = \frac{T}{2}$$

Thus, the gain constant  $K$  becomes  $\frac{1}{2}T$  for sufficiently small values of  $T$ .

### Question 3:

```
% Ogata 1st ed: Problem B-4-1
close all
clear

s = tf('s')

gs = 2/((s+1)*(s+2))

z = tf('z', 0.1)

% Backward difference method
gz1 = 0.01515/(1-1.7424*z^(-1)+0.7576*z^(-2))
% figure
% bode(gs)
% figure
% bode(gz1)
figure
bode(gs,gz1)

% Impulse invariance method
gz2 = 0.01722*z^(-1)/(1-1.7235*z^(-1)+0.7408*z^(-2))
figure
bode(gs,gz2)
```

```
% Ogata 1st ed: Problem B-4-2
```

```
a = 1  
b = 10
```

```
gs2 = (s+a)/(s*(s+b))
```

```
T = 0.2  
z = tf('z', T)
```

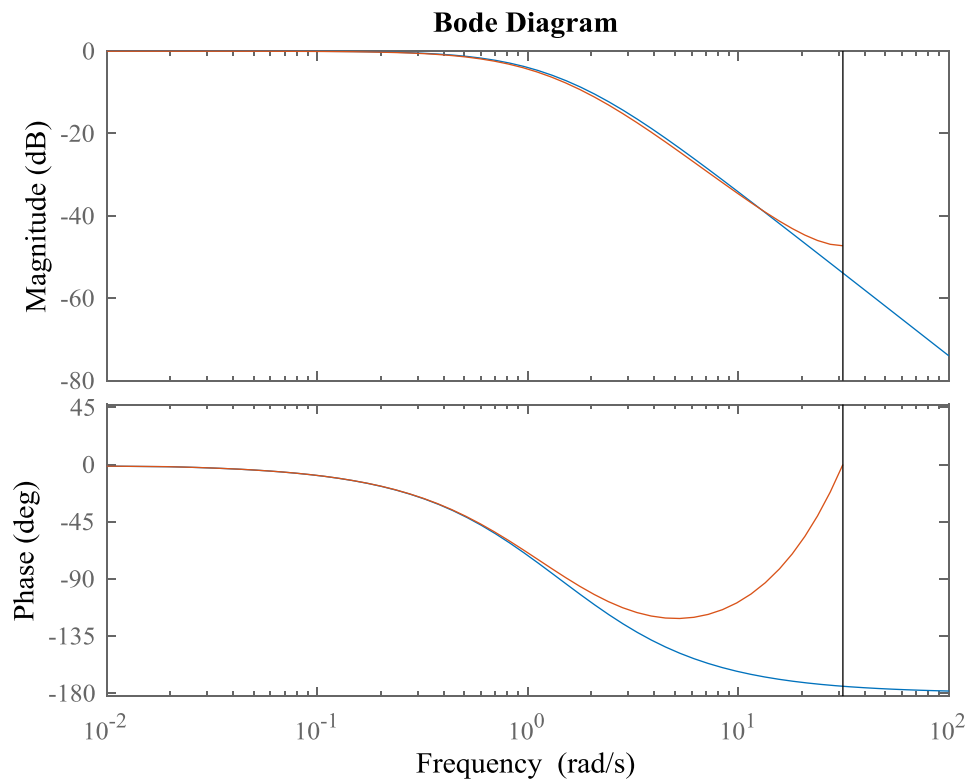
```
% pole-zero mapping method
```

```
gz3 = a*T/(2*b) * (1-exp(-b*T))/(1-exp(-a*T)) * (1+z^(-1))/(1-z^(-1)) * ...  
      (1-exp(-a*T)*z^(-1))/(1-exp(-b*T)*z^(-1))
```

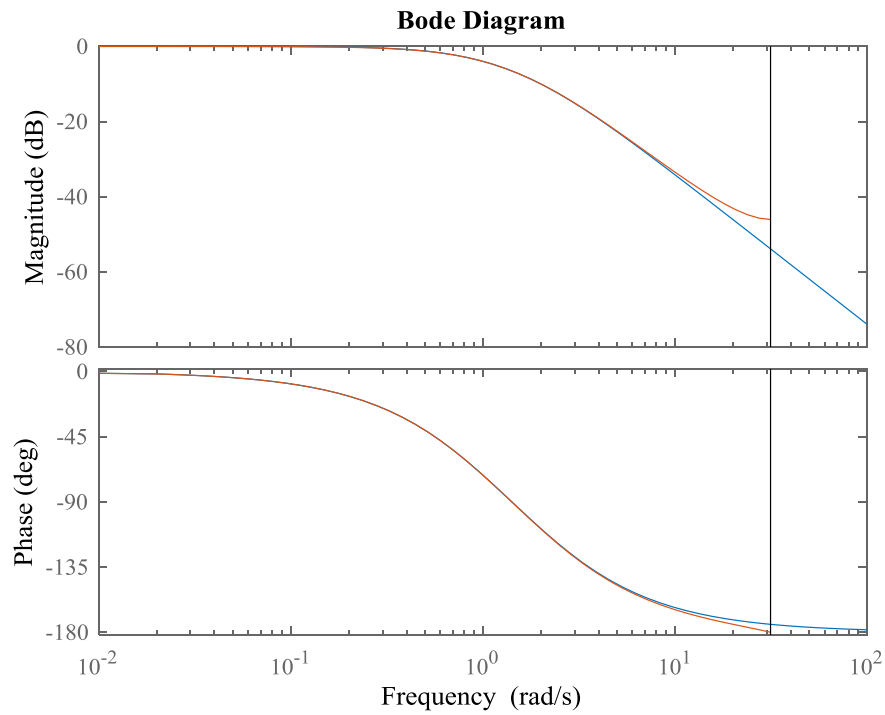
```
figure  
bode(gs2,gz3)
```

Plots from above Matlab code:

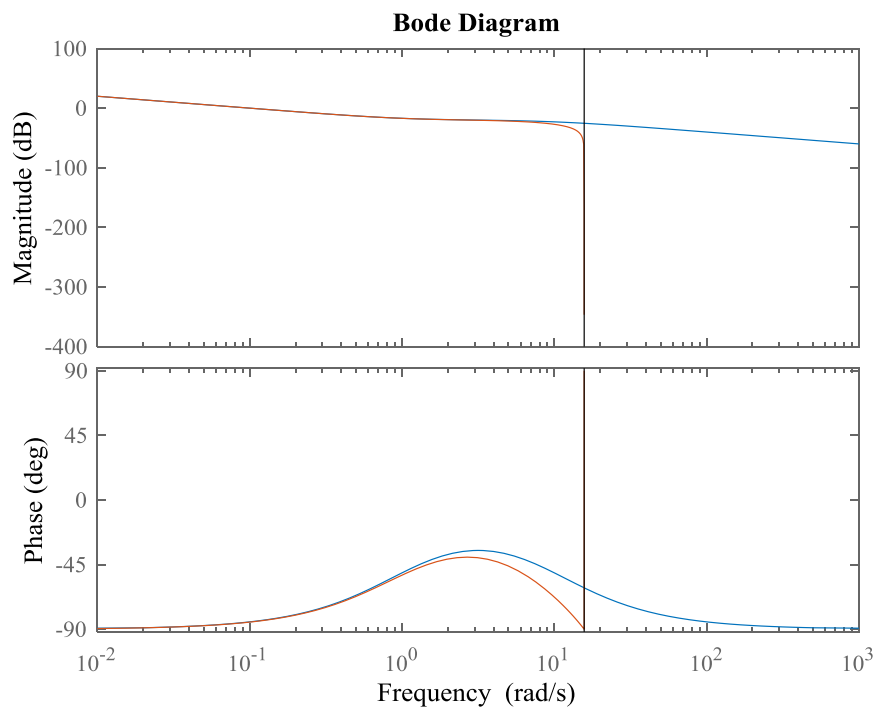
Question 1 using Backward difference method:



Question 1 using `Impulse invariance method`:



Question 2 using `pole-zero mapping method`:



#### Question 4:

B-4-16. For  $T = 0.1$  sec, we have

$$G(z) = \mathcal{Z} \left[ \frac{1 - e^{-Ts}}{s} \frac{5}{(s+1)(s+2)} \right] = (1 - z^{-1}) \mathcal{Z} \left[ \frac{5}{s(s+1)(s+2)} \right]$$

$$= \frac{0.02263(z + 0.9061)}{(z - 0.9048)(z - 0.8187)}$$

Using the transformation

$$z = \frac{1 + \frac{1}{2}Tw}{1 - \frac{1}{2}Tw} = \frac{1 + 0.05w}{1 - 0.05w}$$

we have

$$G(w) = \frac{0.02263 \left( \frac{1 + 0.05w}{1 - 0.05w} + 0.9061 \right)}{\left( \frac{1 + 0.05w}{1 - 0.05w} - 0.9048 \right) \left( \frac{1 + 0.05w}{1 - 0.05w} - 0.8187 \right)}$$

$$= \frac{2.500 \left( 1 - \frac{1}{20} w \right) \left( 1 + \frac{1}{406} w \right)}{(1 + w) \left( 1 + \frac{1}{1.994} w \right)}$$

Notice that in order to have the static velocity error constant  $K_v = 5 \text{ sec}^{-1}$ , we need the controller  $G_D(w)$  to include an integrator.

Using the conventional design approach, we find the following  $G_D(w)$  will satisfy the requirements that the phase margin be  $60^\circ$ , the gain margin be not less than 12 db, and  $K_v$  be equal to  $5 \text{ sec}^{-1}$ .

$$G_D(w) = \frac{2}{w} \left( \frac{1 + \frac{1}{0.1} w}{1 + \frac{1}{0.01} w} \right) \left( \frac{1 + w}{1 + \frac{1}{10} w} \right)$$

Then the open-loop pulse transfer function becomes

$$G_D(w)G(w) = \frac{5}{w} \frac{\left( 1 + \frac{1}{0.1} w \right) \left( 1 - \frac{1}{20} w \right) \left( 1 + \frac{1}{406} w \right)}{\left( 1 + \frac{1}{0.01} w \right) \left( 1 + \frac{1}{10} w \right) \left( 1 + \frac{1}{1.994} w \right)}$$

From the Bode diagram of  $G_D(w)G(w)$  (see next page), we find the phase margin to be approximately  $60^\circ$  and the gain margin to be approximately 22 dB. The gain crossover frequency is  $\nu = 0.5 \text{ rad/sec}$ . The phase crossover frequency is  $\nu = 3.5 \text{ rad/sec}$ .

Next, using the following transformation:

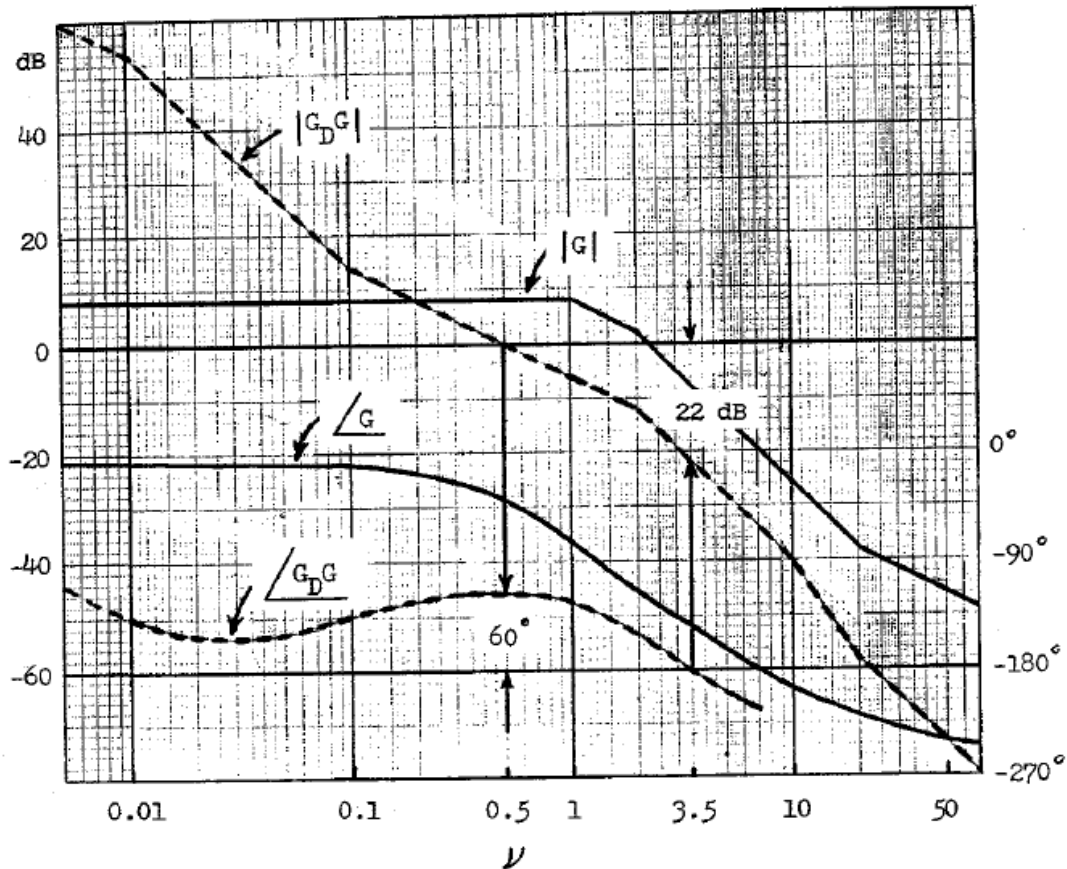
$$w = \frac{2}{0.1} \frac{z - 1}{z + 1} = 20 \frac{z - 1}{z + 1}$$

we obtain  $G_D(z)$  as follows:

$$G_D(z) = \frac{2 \left( 1 + \frac{1}{0.1} 20 \frac{z - 1}{z + 1} \right) \left( 1 + 20 \frac{z - 1}{z + 1} \right)}{20 \left( \frac{z - 1}{z + 1} \right) \left( 1 + \frac{1}{0.01} 20 \frac{z - 1}{z + 1} \right) \left( 1 + \frac{1}{10} 20 \frac{z - 1}{z + 1} \right)}$$

$$= 0.07035 \frac{(z + 1)(z - 0.9900)(z - 0.9048)}{(z - 1)(z - 0.9990)(z - 0.3333)}$$

The digital controller  $G_D(z)$  defined by this last equation satisfies all the requirements of the problem and is, therefore, satisfactory.



#### Matlab code for Question 4:

```
% Ogata Problem B-4-16
close all
clear

s = tf('s')

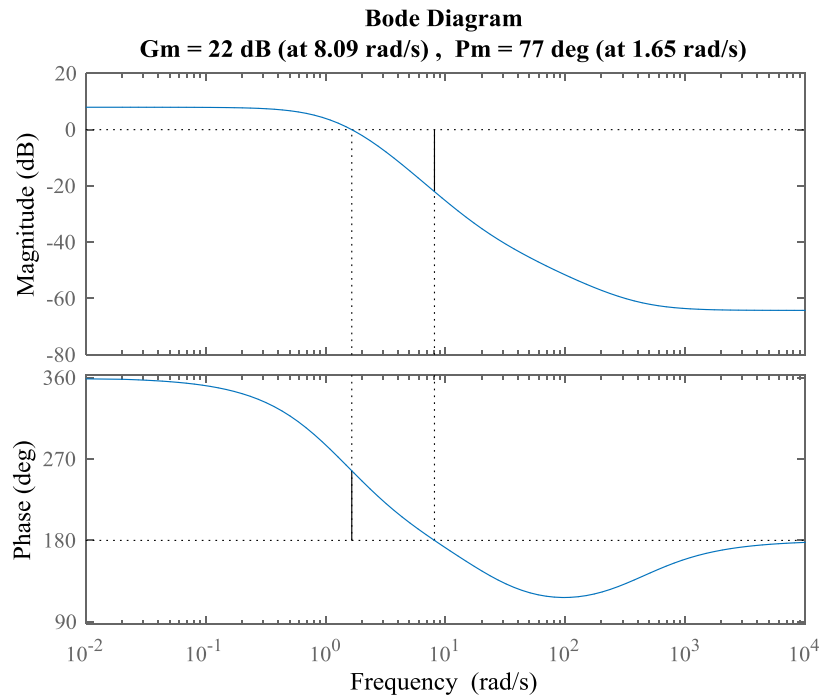
gw = 2.5*(1-s/20)*(1+s/406)/((1+s)*(1+s/1.994))
figure
margin(gw)

gd = 2/s * (1+s/0.1)*(1+s)/((1+s/0.01)*(1+s/10))
figure
margin(gd*gw)

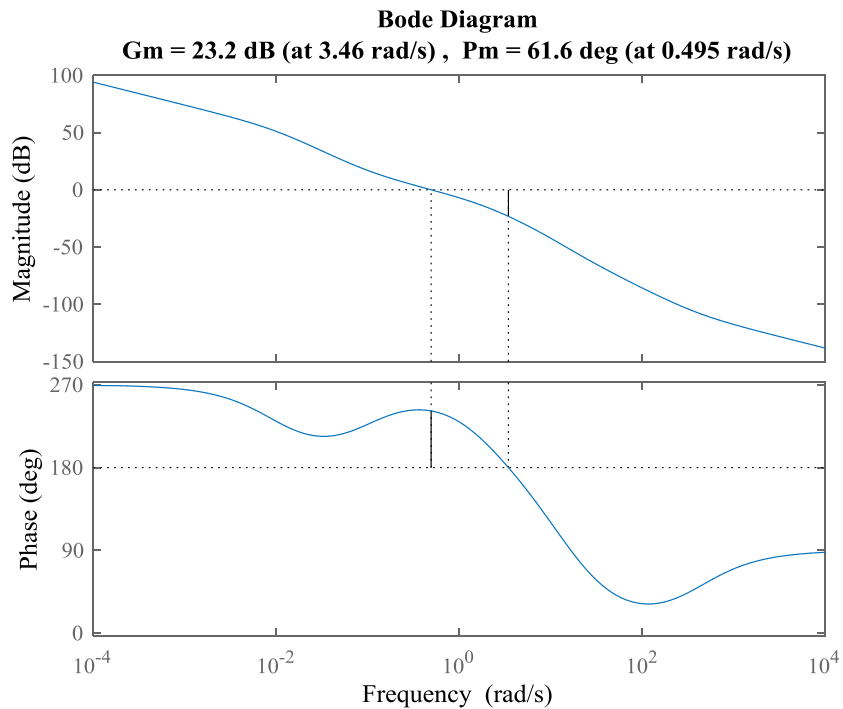
% another solution that has twice the bandwidth
gd = 0.4/s * (1+s)/((1+s/100)) * 5*(1+s/0.05)/(1+s/0.01)
figure
margin(gd*gw)
```

**Results from the above Matlab code:**

**G(w) uncompensated:**



**Compensated loop gain, using the compensator derived above:**





**Compensated loop gain, using an alternative compensator: note the increased bandwidth**

