

Problem 2.27 At an operating frequency of 300 MHz, a lossless 50- Ω air-spaced transmission line 2.5 m in length is terminated with an impedance $Z_L = (40 + j20) \Omega$. Find the input impedance.

Solution: Given a lossless transmission line, $Z_0 = 50 \Omega$, $f = 300 \text{ MHz}$, $l = 2.5 \text{ m}$, and $Z_L = (40 + j20) \Omega$. Since the line is air filled, $u_p = c$ and therefore, from Eq. (2.48),

$$\beta = \frac{\omega}{u_p} = \frac{2\pi \times 300 \times 10^6}{3 \times 10^8} = 2\pi \text{ rad/m.}$$

Since the line is lossless, Eq. (2.79) is valid:

$$\begin{aligned} Z_{\text{in}} &= Z_0 \left(\frac{Z_L + jZ_0 \tan \beta l}{Z_0 + jZ_L \tan \beta l} \right) = 50 \left[\frac{(40 + j20) + j50 \tan(2\pi \text{ rad/m} \times 2.5 \text{ m})}{50 + j(40 + j20) \tan(2\pi \text{ rad/m} \times 2.5 \text{ m})} \right] \\ &= 50 [(40 + j20) + j50 \times 0] / [50 + j(40 + j20) \times 0] \\ &= (40 + j20) \Omega. \end{aligned}$$

Problem 2.28 A lossless transmission line of electrical length $l = 0.35\lambda$ is terminated in a load impedance as shown in Fig. P2.28. Find Γ , S , and Z_{in} . Verify your results using CD Modules 2.4 or 2.5. Include a printout of the screen's output display.

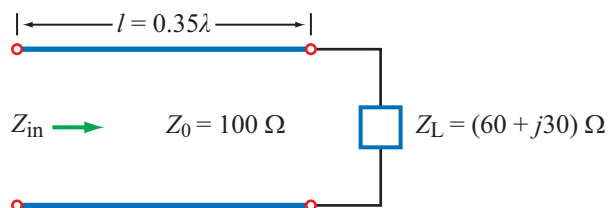


Figure P2.28: Circuit for Problem 2.28.

Solution: From Eq. (2.59),

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{(60 + j30) - 100}{(60 + j30) + 100} = 0.307e^{j132.5^\circ}.$$

From Eq. (2.73),

$$S = \frac{1 + |\Gamma|}{1 - |\Gamma|} = \frac{1 + 0.307}{1 - 0.307} = 1.89.$$

From Eq. (2.79)

$$\begin{aligned} Z_{in} &= Z_0 \left(\frac{Z_L + jZ_0 \tan \beta l}{Z_0 + jZ_L \tan \beta l} \right) \\ &= 100 \left[\frac{(60 + j30) + j100 \tan \left(\frac{2\pi \text{ rad}}{\lambda} 0.35\lambda \right)}{100 + j(60 + j30) \tan \left(\frac{2\pi \text{ rad}}{\lambda} 0.35\lambda \right)} \right] = (64.8 - j38.3) \Omega. \end{aligned}$$

Module 2.4
Transmission Line Simulator
Options:

d = λ

$Z_L = 60.0 + j 30.0 \ \Omega$
 $f = 3.75 \ \text{GHz}$
 $\lambda = 80.0 \ \text{mm}$

Set Line

Length units: [λ] [m]

Low Loss Approximation

Characteristic Impedance $Z_0 =$ Ω

Frequency $f =$ Hz

Relative Permittivity $\epsilon_r =$

Line Length $l =$ [λ]

$Z_L =$ + j Ω

Impedance Admittance

Set Generator

$\tilde{V}_g =$ + j V

$Z_g =$ + j Ω

Output

Transmission Line Data 1

Cursor $d = 0.35 \ \lambda = 28.0 \ \text{mm}$

Impedance [Ω]	$Z(d) = 64.841222 - j 38.282867$ $= 75.29915 \ \angle -0.5333 \ \text{rad}$
Admittance [S]	$Y(d) = 0.011436 + j 0.006752$ $= 0.01328 \ \angle 0.5333 \ \text{rad}$
Reflection Coefficient	$\Gamma_d = -0.15119794 - j 0.2673552$ $= 0.30714756 \ \angle -2.085486 \ \text{rad}$ $= 0.30714756 \ \angle -119.489553^\circ$
Voltage [V]	$\tilde{V}(d) = 0.60816 - j 0.130622$ $= 0.622029 \ \angle -0.2116 \ \text{rad}$
Current [A]	$\tilde{I}(d) = 0.007837 + j 0.002612$ $= 0.008261 \ \angle 0.3218 \ \text{rad}$
Power Flow [mW]	$P_{av} = 2.212394$

Problem 2.32 A 6-m section of 150- Ω lossless line is driven by a source with

$$v_g(t) = 5 \cos(8\pi \times 10^7 t - 30^\circ) \quad (\text{V})$$

and $Z_g = 150 \Omega$. If the line, which has a relative permittivity $\epsilon_r = 2.25$, is terminated in a load $Z_L = (150 - j50) \Omega$, determine:

- λ on the line.
- The reflection coefficient at the load.
- The input impedance.
- The input voltage \tilde{V}_i .
- The time-domain input voltage $v_i(t)$.
- Quantities in (a) to (d) using CD Modules 2.4 or 2.5.

Solution:

$$v_g(t) = 5 \cos(8\pi \times 10^7 t - 30^\circ) \text{ V},$$

$$\tilde{V}_g = 5e^{-j30^\circ} \text{ V}.$$

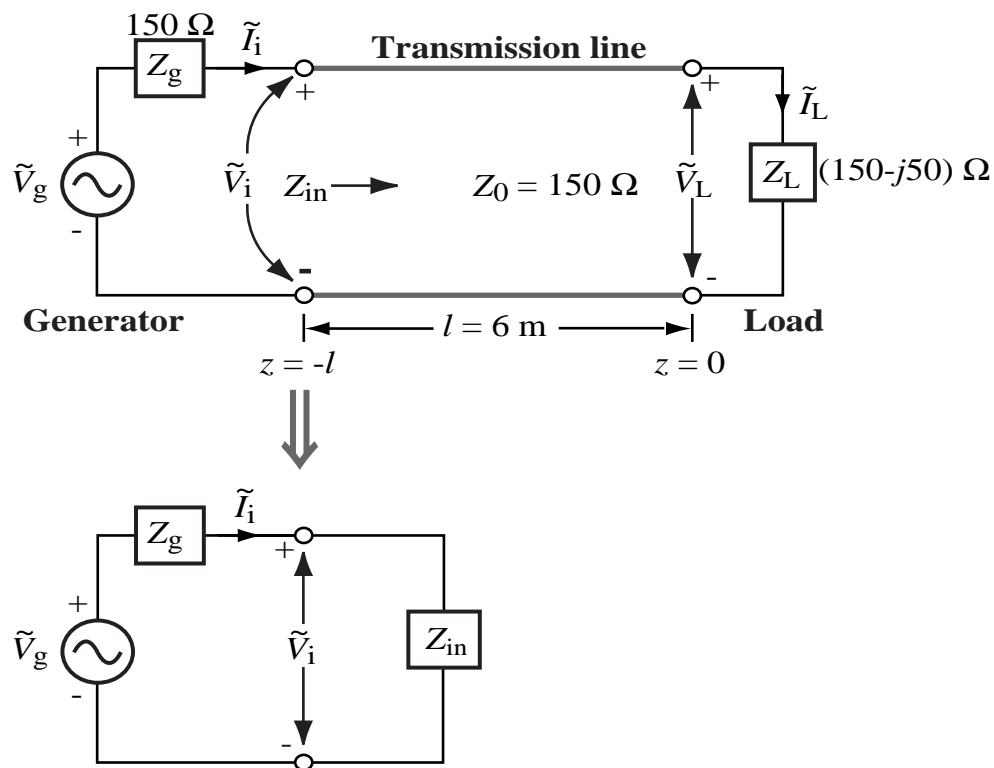


Figure P2.32: Circuit for Problem 2.32.

(a)

$$\begin{aligned}u_p &= \frac{c}{\sqrt{\epsilon_r}} = \frac{3 \times 10^8}{\sqrt{2.25}} = 2 \times 10^8 \quad (\text{m/s}), \\ \lambda &= \frac{u_p}{f} = \frac{2\pi u_p}{\omega} = \frac{2\pi \times 2 \times 10^8}{8\pi \times 10^7} = 5 \text{ m}, \\ \beta &= \frac{\omega}{u_p} = \frac{8\pi \times 10^7}{2 \times 10^8} = 0.4\pi \quad (\text{rad/m}), \\ \beta l &= 0.4\pi \times 6 = 2.4\pi \quad (\text{rad}).\end{aligned}$$

Since this exceeds 2π (rad), we can subtract 2π , which leaves a remainder $\beta l = 0.4\pi$ (rad).

(b) $\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{150 - j50 - 150}{150 - j50 + 150} = \frac{-j50}{300 - j50} = 0.16e^{-j80.54^\circ}$.

(c)

$$\begin{aligned}Z_{\text{in}} &= Z_0 \left[\frac{Z_L + jZ_0 \tan \beta l}{Z_0 + jZ_L \tan \beta l} \right] \\ &= 150 \left[\frac{(150 - j50) + j150 \tan(0.4\pi)}{150 + j(150 - j50) \tan(0.4\pi)} \right] = (115.70 + j27.42) \Omega.\end{aligned}$$

(d)

$$\begin{aligned}\tilde{V}_i &= \frac{\tilde{V}_g Z_{\text{in}}}{Z_g + Z_{\text{in}}} = \frac{5e^{-j30^\circ} (115.7 + j27.42)}{150 + 115.7 + j27.42} \\ &= 5e^{-j30^\circ} \left(\frac{115.7 + j27.42}{265.7 + j27.42} \right) \\ &= 5e^{-j30^\circ} \times 0.44e^{j7.44^\circ} = 2.2e^{-j22.56^\circ} \quad (\text{V}).\end{aligned}$$

(e)

$$v_i(t) = \Re\{\tilde{V}_i e^{j\omega t}\} = \Re\{2.2e^{-j22.56^\circ} e^{j\omega t}\} = 2.2 \cos(8\pi \times 10^7 t - 22.56^\circ) \text{ V}.$$

Module 2.4 Transmission Line Simulator Options: Set Input / Output

d =

$d = 1.2 \lambda = 6.0 \text{ m}$ $Z_L = 150.0 - j 50.0 \ \Omega$

$Z_g = 150.0 + j 0.0 \ \Omega$ $Z_0 = 150.0 + j 0.0 \ \Omega$ $f = 40.0 \text{ MHz}$
 $\bar{V}_g = 4.33 - j 2.5 \text{ V}$ $\epsilon_r = 2.25$ $\lambda = 5.0 \text{ m}$

$d = 1.2 \lambda = 6.0 \text{ m}$ $d = 0$

Set Line
Length units: [λ] [m]

Low Loss Approximation

Characteristic Impedance $Z_0 = 150 \ \Omega$
 Frequency $f = 4E7 \text{ Hz}$
 Relative Permittivity $\epsilon_r = 2.25$
 Line Length $l = 6 \text{ [m]}$

$Z_L = 150 + j -50 \ \Omega$

Impedance Admittance

Set Generator

$\bar{V}_g = 4.33 + j -2.5 \text{ V}$
 $Z_g = 150 + j 0.0 \ \Omega$

Output Transmission Line Data 1

Cursor $d = 1.2 \lambda = 6.0 \text{ m}$

Impedance $Z(d) = 115.702409 + j 27.423507 \ \Omega$
 $= 118.907931 \ \angle 0.2327 \text{ rad}$

Admittance $Y(d) = 0.008183 - j 0.00194 \text{ [S]}$
 $= 0.00841 \ \angle -0.2327 \text{ rad}$

Reflection Coefficient $\Gamma_d = -0.11718185 + j 0.11530585$
 $= 0.16439899 \ \angle 2.364264 \text{ rad}$
 $= 0.16439899 \ \angle 135.462322^\circ$

Voltage $V(d) = 2.055434 - j 0.853886 \text{ [V]}$
 $= 2.225742 \ \angle -0.3937 \text{ rad}$

Current $I(d) = 0.015164 - j 0.010974 \text{ [A]}$
 $= 0.018718 \ \angle -0.6265 \text{ rad}$

Power Flow $P_{av} = 20.269378 \text{ [mW]}$

5 cos (-30)

5 sin(-30)

Problem 2.41 A $50\text{-}\Omega$ lossless line of length $l = 0.375\lambda$ connects a 300-MHz generator with $\tilde{V}_g = 300\text{ V}$ and $Z_g = 50\text{ }\Omega$ to a load Z_L . Determine the time-domain current through the load for:

- (a) $Z_L = (50 - j50)\text{ }\Omega$
- (b) $Z_L = 50\text{ }\Omega$
- (c) $Z_L = 0$ (short circuit)

For (a), verify your results by deducing the information you need from the output products generated by CD Module 2.4.

Solution:

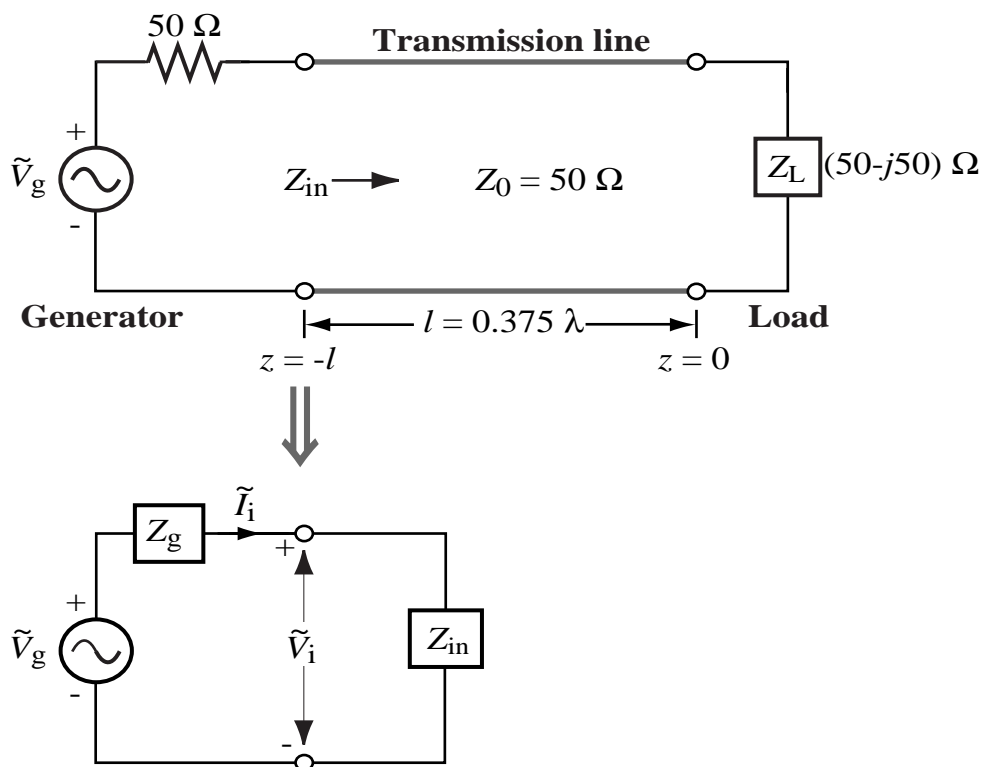


Figure P2.41: Circuit for Problem 2.41(a).

- (a) $Z_L = (50 - j50)\text{ }\Omega$, $\beta l = \frac{2\pi}{\lambda} \times 0.375\lambda = 2.36\text{ (rad)} = 135^\circ$.

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{50 - j50 - 50}{50 - j50 + 50} = \frac{-j50}{100 - j50} = 0.45 e^{-j63.43^\circ}.$$

Application of Eq. (2.79) gives:

$$Z_{\text{in}} = Z_0 \left[\frac{Z_L + jZ_0 \tan \beta l}{Z_0 + jZ_L \tan \beta l} \right] = 50 \left[\frac{(50 - j50) + j50 \tan 135^\circ}{50 + j(50 - j50) \tan 135^\circ} \right] = (100 + j50) \Omega.$$

Using Eq. (2.82) gives

$$\begin{aligned} V_0^+ &= \left(\frac{\tilde{V}_g Z_{\text{in}}}{Z_g + Z_{\text{in}}} \right) \left(\frac{1}{e^{j\beta l} + \Gamma e^{-j\beta l}} \right) \\ &= \frac{300(100 + j50)}{50 + (100 + j50)} \left(\frac{1}{e^{j135^\circ} + 0.45 e^{-j63.43^\circ} e^{-j135^\circ}} \right) \\ &= 150 e^{-j135^\circ} \quad (\text{V}), \\ \tilde{I}_L &= \frac{V_0^+}{Z_0} (1 - \Gamma) = \frac{150 e^{-j135^\circ}}{50} (1 - 0.45 e^{-j63.43^\circ}) = 2.68 e^{-j108.44^\circ} \quad (\text{A}), \\ i_L(t) &= \Re \{ \tilde{I}_L e^{j\omega t} \} \\ &= \Re \{ 2.68 e^{-j108.44^\circ} e^{j6\pi \times 10^8 t} \} \\ &= 2.68 \cos(6\pi \times 10^8 t - 108.44^\circ) \quad (\text{A}). \end{aligned}$$

(b)

$$\begin{aligned} Z_L &= 50 \Omega, \\ \Gamma &= 0, \\ Z_{\text{in}} &= Z_0 = 50 \Omega, \\ V_0^+ &= \frac{300 \times 50}{50 + 50} \left(\frac{1}{e^{j135^\circ} + 0} \right) = 150 e^{-j135^\circ} \quad (\text{V}), \\ \tilde{I}_L &= \frac{V_0^+}{Z_0} = \frac{150}{50} e^{-j135^\circ} = 3 e^{-j135^\circ} \quad (\text{A}), \\ i_L(t) &= \Re \{ 3 e^{-j135^\circ} e^{j6\pi \times 10^8 t} \} = 3 \cos(6\pi \times 10^8 t - 135^\circ) \quad (\text{A}). \end{aligned}$$

(c)

$$\begin{aligned} Z_L &= 0, \\ \Gamma &= -1, \\ Z_{\text{in}} &= Z_0 \left(\frac{0 + jZ_0 \tan 135^\circ}{Z_0 + 0} \right) = jZ_0 \tan 135^\circ = -j50 \quad (\Omega), \\ V_0^+ &= \frac{300(-j50)}{50 - j50} \left(\frac{1}{e^{j135^\circ} - e^{-j135^\circ}} \right) = 150 e^{-j135^\circ} \quad (\text{V}), \end{aligned}$$

$$\tilde{I}_L = \frac{V_0^+}{Z_0} [1 - \Gamma] = \frac{150 e^{-j135^\circ}}{50} [1 + 1] = 6 e^{-j135^\circ} \quad (\text{A}),$$

$$i_L(t) = 6 \cos(6\pi \times 10^8 t - 135^\circ) \quad (\text{A}).$$

From output of Module 2.4, at $d = 0$ (load)

$$\tilde{I}(d) = 2.68 \angle -1.89 \text{ rad},$$

which corresponds to

$$\tilde{I}(d) = 2.68 \angle -108.29^\circ.$$

The equivalent time-domain current at $f = 300$ MHz is

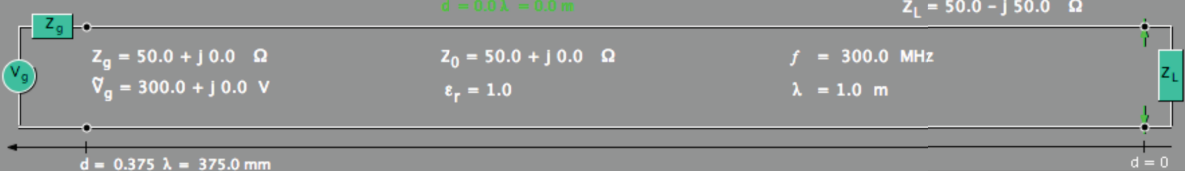
$$i_L(t) = 2.68 \cos(6\pi \times 10^8 t - 108.29^\circ) \quad (\text{A}).$$

Module 2.4

Transmission Line Simulator

Options: Set Input / Output

d = λ



$d = 0.375 \lambda = 375.0 \text{ mm}$

$d = 0.0 \lambda = 0.0 \text{ m}$

$Z_L = 50.0 - j 50.0 \ \Omega$

$Z_g = 50.0 + j 0.0 \ \Omega$

$\tilde{V}_g = 300.0 + j 0.0 \text{ V}$

$Z_0 = 50.0 + j 0.0 \ \Omega$

$\epsilon_r = 1.0$

$f = 300.0 \text{ MHz}$

$\lambda = 1.0 \text{ m}$

Set Line

Length units: [λ] [m]

Low Loss Approximation

Characteristic Impedance $Z_0 =$ Ω

Frequency $f =$ Hz

Relative Permittivity $\epsilon_r =$

Line Length $l =$ λ

$Z_L =$ + j Ω

Impedance Admittance

Set Generator

$\tilde{V}_g =$ + j V

$Z_g =$ + j Ω

Output Transmission Line Data 1

Cursor $d = 0.0 \lambda = 0.0 \text{ m}$

Impedance $Z(d) = 50.0 - j 50.0$
= 70.710678 L -0.7854 rad

Admittance $Y(d) = 0.01 + j 0.01$
= 0.014142 L 0.7854 rad

Reflection Coefficient $\Gamma_d = 0.2 - j 0.4$
= 0.4472136 L -1.107149 rad
= 0.4472136 L -63.434949°

Voltage $\tilde{V}(d) = -169.705627 - j 84.852814$
= 189.73666 L -2.6779 rad

Current $\tilde{I}(d) = -0.848528 - j 2.545584$
= 2.683282 L -1.8925 rad

Power Flow $P_{av} = 180.0$

Problem 2.42 A generator with $\tilde{V}_g = 300$ V and $Z_g = 50 \Omega$ is connected to a load $Z_L = 75 \Omega$ through a $50\text{-}\Omega$ lossless line of length $l = 0.15\lambda$.

- Compute Z_{in} , the input impedance of the line at the generator end.
- Compute \tilde{I}_i and \tilde{V}_i .
- Compute the time-average power delivered to the line, $P_{in} = \frac{1}{2}\Re[\tilde{V}_i\tilde{I}_i^*]$.
- Compute \tilde{V}_L , \tilde{I}_L , and the time-average power delivered to the load, $P_L = \frac{1}{2}\Re[\tilde{V}_L\tilde{I}_L^*]$. How does P_{in} compare to P_L ? Explain.
- Compute the time-average power delivered by the generator, P_g , and the time-average power dissipated in Z_g . Is conservation of power satisfied?

Solution:

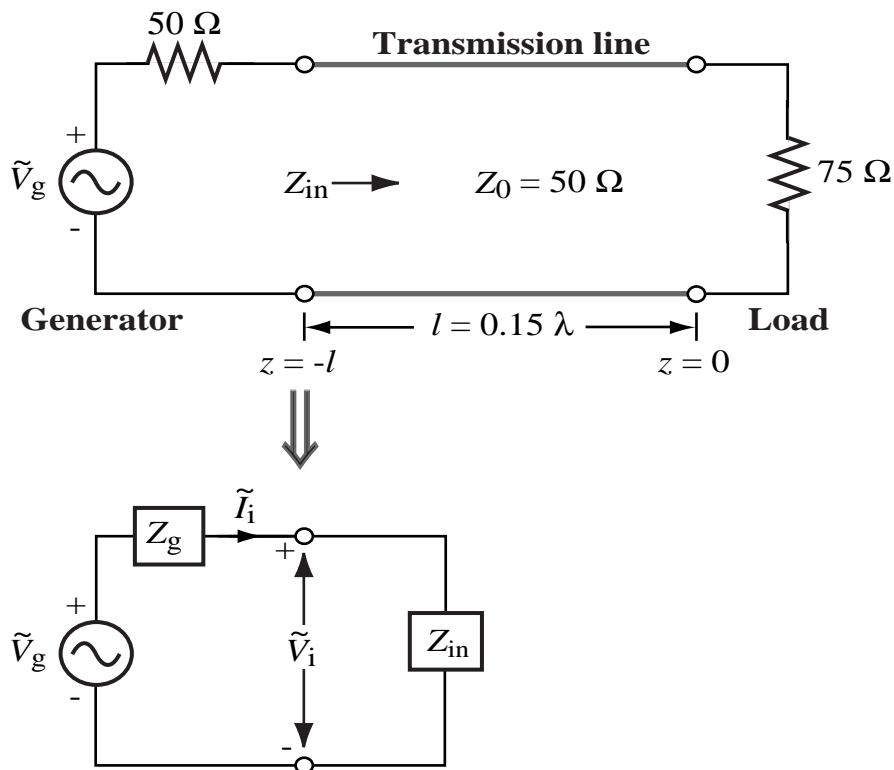


Figure P2.42: Circuit for Problem 2.42.

(a)

$$\beta l = \frac{2\pi}{\lambda} \times 0.15\lambda = 54^\circ,$$

$$Z_{\text{in}} = Z_0 \left[\frac{Z_L + jZ_0 \tan \beta l}{Z_0 + jZ_L \tan \beta l} \right] = 50 \left[\frac{75 + j50 \tan 54^\circ}{50 + j75 \tan 54^\circ} \right] = (41.25 - j16.35) \Omega.$$

(b)

$$\tilde{I}_i = \frac{\tilde{V}_g}{Z_g + Z_{\text{in}}} = \frac{300}{50 + (41.25 - j16.35)} = 3.24 e^{j10.16^\circ} \quad (\text{A}),$$

$$\tilde{V}_i = \tilde{I}_i Z_{\text{in}} = 3.24 e^{j10.16^\circ} (41.25 - j16.35) = 143.6 e^{-j11.46^\circ} \quad (\text{V}).$$

(c)

$$\begin{aligned} P_{\text{in}} &= \frac{1}{2} \Re[\tilde{V}_i \tilde{I}_i^*] = \frac{1}{2} \Re[143.6 e^{-j11.46^\circ} \times 3.24 e^{-j10.16^\circ}] \\ &= \frac{143.6 \times 3.24}{2} \cos(21.62^\circ) = 216 \quad (\text{W}). \end{aligned}$$

(d)

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{75 - 50}{75 + 50} = 0.2,$$

$$V_0^+ = \tilde{V}_i \left(\frac{1}{e^{j\beta l} + \Gamma e^{-j\beta l}} \right) = \frac{143.6 e^{-j11.46^\circ}}{e^{j54^\circ} + 0.2 e^{-j54^\circ}} = 150 e^{-j54^\circ} \quad (\text{V}),$$

$$\tilde{V}_L = V_0^+ (1 + \Gamma) = 150 e^{-j54^\circ} (1 + 0.2) = 180 e^{-j54^\circ} \quad (\text{V}),$$

$$\tilde{I}_L = \frac{V_0^+}{Z_0} (1 - \Gamma) = \frac{150 e^{-j54^\circ}}{50} (1 - 0.2) = 2.4 e^{-j54^\circ} \quad (\text{A}),$$

$$P_L = \frac{1}{2} \Re[\tilde{V}_L \tilde{I}_L^*] = \frac{1}{2} \Re[180 e^{-j54^\circ} \times 2.4 e^{j54^\circ}] = 216 \quad (\text{W}).$$

$P_L = P_{\text{in}}$, which is as expected because the line is lossless; power input to the line ends up in the load.

(e)

Power delivered by generator:

$$P_g = \frac{1}{2} \Re[\tilde{V}_g \tilde{I}_i] = \frac{1}{2} \Re[300 \times 3.24 e^{j10.16^\circ}] = 486 \cos(10.16^\circ) = 478.4 \quad (\text{W}).$$

Power dissipated in Z_g :

$$P_{Z_g} = \frac{1}{2} \Re[\tilde{I}_i \tilde{V}_{Z_g}] = \frac{1}{2} \Re[\tilde{I}_i \tilde{I}_i^* Z_g] = \frac{1}{2} |\tilde{I}_i|^2 Z_g = \frac{1}{2} (3.24)^2 \times 50 = 262.4 \quad (\text{W}).$$

Note 1: $P_g = P_{Z_g} + P_{\text{in}} = 478.4 \text{ W}$.

Problem 2.75 Generate a bounce diagram for the voltage $V(z, t)$ for a 1-m-long lossless line characterized by $Z_0 = 50 \Omega$ and $u_p = 2c/3$ (where c is the velocity of light) if the line is fed by a step voltage applied at $t = 0$ by a generator circuit with $V_g = 60 \text{ V}$ and $R_g = 100 \Omega$. The line is terminated in a load $R_L = 25 \Omega$. Use the bounce diagram to plot $V(t)$ at a point midway along the length of the line from $t = 0$ to $t = 25 \text{ ns}$.

Solution:

$$\Gamma_g = \frac{R_g - Z_0}{R_g + Z_0} = \frac{100 - 50}{100 + 50} = \frac{50}{150} = \frac{1}{3},$$

$$\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{25 - 50}{25 + 50} = \frac{-25}{75} = -\frac{1}{3}.$$

From Eq. (2.149b),

$$V_1^+ = \frac{V_g Z_0}{R_g + Z_0} = \frac{60 \times 50}{100 + 50} = 20 \text{ V}.$$

Also,

$$T = \frac{l}{u_p} = \frac{l}{2c/3} = \frac{3}{2 \times 3 \times 10^8} = 5 \text{ ns}.$$

The bounce diagram is shown in Fig. P2.75(a) and the plot of $V(t)$ in Fig. P2.75(b).

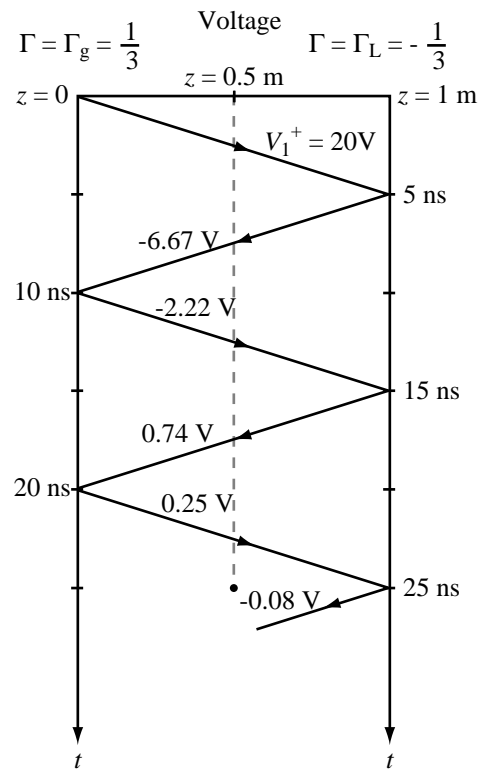


Figure P2.75: (a) Bounce diagram for Problem 2.75.

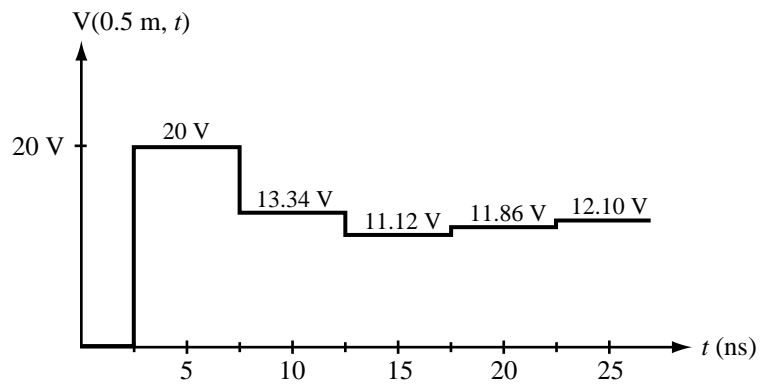


Figure P2.75: (b) Time response of voltage.

Problem 2.78 In response to a step voltage, the voltage waveform shown in Fig. P2.78 was observed at the sending end of a shorted line with $Z_0 = 50 \Omega$ and $\epsilon_r = 4$. Determine V_g , R_g , and the line length.

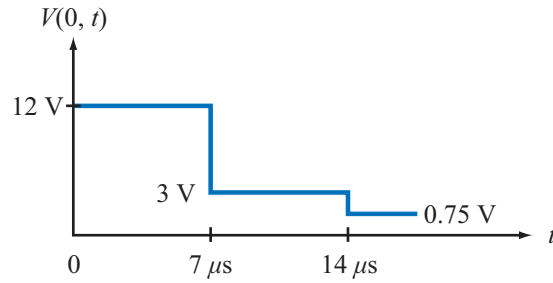


Figure P2.78: Voltage waveform of Problem 2.78.

Solution:

$$u_p = \frac{c}{\sqrt{\epsilon_r}} = \frac{3 \times 10^8}{\sqrt{4}} = 1.5 \times 10^8 \text{ m/s},$$

$$7 \mu\text{s} = 7 \times 10^{-6} \text{ s} = \frac{2l}{u_p} = \frac{2l}{1.5 \times 10^8}.$$

Hence, $l = 525 \text{ m}$.

From the voltage waveform, $V_1^+ = 12 \text{ V}$. At $t = 7 \mu\text{s}$, the voltage at the sending end is

$$V(z=0, t=7 \mu\text{s}) = V_1^+ + \Gamma_L V_1^+ + \Gamma_g \Gamma_L V_1^+ = -\Gamma_g V_1^+ \quad (\text{because } \Gamma_L = -1).$$

Hence, $3 \text{ V} = -\Gamma_g \times 12 \text{ V}$, or $\Gamma_g = -0.25$. From Eq. (2.153),

$$R_g = Z_0 \left(\frac{1 + \Gamma_g}{1 - \Gamma_g} \right) = 50 \left(\frac{1 - 0.25}{1 + 0.25} \right) = 30 \Omega.$$

Also,

$$V_1^+ = \frac{V_g Z_0}{R_g + Z_0}, \quad \text{or} \quad 12 = \frac{V_g \times 50}{30 + 50},$$

which gives $V_g = 19.2 \text{ V}$.
